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ANTENNA EMBLEMS RESHAPED AS ICONS AND AESTHETIC LOGOS (AERIAL)

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ABSTRACT: This paper introduces the concept of designing microstrip patch antennas to take the form of aesthetic arbitrary shapes or logos. Various intermediate shapes have been examined to analyze the behavior of asymmetric, curved, angular and disconnected sections.

Key Words: Logo, aesthetic design, microstrip patch antenna

1. INTRODUCTION

Antennas and wireless connectivity are essential to our everyday activity. However, antennas are generally functional objects that need to be miniaturised and hidden to avoid hindering the aesthetics of the product in which it is incorporated into. This means compromising the antenna in terms of size which limits the inherent efficiency and bandwidth due to the Wheeler-Chu limits [1]. Surrounding materials and non-ideal placement also compromise electromagnetic performance. Conversely, if the antenna was an aesthetic shape, for example a flower, a smiley face or even a company logo, these restrictions would be negated. This concept lends itself particularly to wearable technology where conducting threads can be used to embroider antennas [2]. This new approach to antenna design could be particularly attractive to companies as it reinforces technology and functionality with a recognised brand to create a unique product. The technology itself would also be protected by copyright and registered design rights.

Microstrip patch antennas are popular due to their low profile; ease of construction and the isolation from other objects due to the ground plane [3]. Different geometries have been considered including square, triangular rectangular, circular, elliptical, slots and parasitic elements [4], [5]. However, these shapes were optimised for their electromagnetic performance and the aesthetic aspects were not considered.

Logo-based antennas have recently been considered [6–9]. These were monopole and dipole antennas and hence would be detuned in the presence of nearby metal objects. The original shapes were modified and they required an element of symmetry in the design. In [6], a logo design was placed inside a circle but it was predominantly the circle which acted as the antenna and not the logo. In [7] and [8] the impedance match of a text logo was changed by modifying the shape of connected letters. A text-based dipole RFID antenna has been created by physically connecting individual letters [9]. In a related area, capacitive coupling between distinct structures has been studied [10].
2. SIMULATED RESULTS

Six variations of the Loughborough University (LU) Shield were considered and are shown in Fig. 1. This logo was chosen as it includes asymmetry and disconnected sections – however the design rules can be applied to any number of aesthetic or logo shapes. All the antennas were fed from the left hand side – the feedpoint was moved to obtain the best match for each case. A probe feed was utilised in order to avoid changing the shape of the logo with an added transmission line feed. The patch antennas were placed above a 1.6mm thick substrate ($\varepsilon_r = 4.5$; tan delta = 0.001). The ground plane size was 120 × 120mm. To allow a fair comparison, the size and aspect ratios of the different patches were fixed at 60mm high which meant the width was 50.36mm.

The logo antennas were simulated using EMPIRE finite-difference time-domain (FDTD) software. The shapes were converted into a single-colour 2D image (jpeg format). Commercial CAD software was then used to convert the image into a 3D STL file with thickness 0.1mm. Care was taken to mesh the curved structures finely.

Fig. 1. The geometry of the six patches including the surface currents at the resonance frequency: (a) rectangular; (b) L-shape; (c) L-shape with square; (d) shield; (e) L-shaped shield and (f) LU Shield

The return loss results are shown in Fig. 2. As expected, the antennas could be tuned to a particular frequency by scaling their size. By examining the surface currents and S11 results, the disconnected square had negligible effect at the principal resonance and a marginally larger effect at higher frequencies. However, the square did change the 50 ohm impedance point.
The performance of the different antennas is compared in Table 1. The bandwidth and efficiency could be improved by using a thicker substrate with a lower permittivity. The L-shaped antennas produced longer current paths and hence resonated at a lower frequency (see Fig. 1); consequently the efficiency and fractional bandwidth (FBW) were reduced. Note, comparable efficiency and bandwidth results were obtained for the rectangular patch when a higher permittivity substrate was used to reduce the frequency. The LU Shield had similar performance compared to the angular or curved L-shaped antennas. The second resonance of the LU Shield (at 1836MHz) had an efficiency of 85%. The cross and co-polar patterns (not included for space reasons) were slightly tilted due to the asymmetric shape but the overall magnitude is reasonably omnidirectional in the azimuth plane.

**Table 1: Simulated performance of the six patch antennas**

<table>
<thead>
<tr>
<th>Antenna geometry</th>
<th>Freq $F_0$ (MHz)</th>
<th>10dB BW (MHz)</th>
<th>Gain at $F_0$ (dBi)</th>
<th>Eff. at $F_0$ (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Rectangle</td>
<td>1358</td>
<td>12</td>
<td>5.85</td>
<td>80.6</td>
</tr>
<tr>
<td>L–shape</td>
<td>978</td>
<td>4</td>
<td>2.81</td>
<td>46.9</td>
</tr>
<tr>
<td>L-shape with square</td>
<td>979</td>
<td>4</td>
<td>2.33</td>
<td>42.2</td>
</tr>
<tr>
<td>Shield</td>
<td>1445</td>
<td>11</td>
<td>6.17</td>
<td>86.1</td>
</tr>
<tr>
<td>L-shaped shield</td>
<td>1044</td>
<td>3</td>
<td>2.46</td>
<td>42.4</td>
</tr>
<tr>
<td>LU Shield</td>
<td>1045</td>
<td>4</td>
<td>3.41</td>
<td>52.6</td>
</tr>
</tbody>
</table>

**3. MEASURED RESULTS**

The LU Shield was etched on an FR4 substrate ($\varepsilon_r = 4.5$; tan delta = 0.02) as shown in Fig. 3. A hole was drilled through the ground, substrate and patch and the inner pin of an SMA connector was soldered to the top of the patch. The measured results showed excellent agreement with the simulations as shown in Fig. 4.
Fig. 3. The fabricated LU Shield antenna on an FR4 substrate

Fig. 4. Simulated and measured return loss of the LU Shield

4. CONCLUSIONS

This paper has demonstrated that it is possible to reconsider how we design antennas by giving greater importance to the aesthetic qualities of the design. Although, using a pre-defined shape may not be the optimal antenna design, this can be counteracted by removing the size and cluttered-environmental constraints. Each shape or logo will present different technical challenges but can be analysed using similar principles.
Complex and detailed shapes will lengthen the current path, thereby reducing the frequency. The shapes can then be scaled to the desired frequency. Intricate shapes will exhibit comparable performance to the basic geometric shape. The optimal feedpoint location must be found for each geometry.

A particular challenge is to design antennas when the logo consists of disconnected sections. In certain cases, these parasitic elements could produce wideband or multiband operation. The coupling of discrete shapes will be determined by the direction of current flow, the size of the gap and the frequency. However, in most cases, the coupling will be small and the disconnected section can be made of either metallic or non-metallic materials. Additional simulations related to this paper demonstrated that connecting the disconnected section to the main antenna element with thin strips was possible, but the modified structure did not behave like a continuous patch. Asymmetry in the design introduces a small degree of beam tilt. However, in many situations such as wearable antennas, the presence of the body will result in larger alterations to the radiation patterns.

5. ACKNOWLEDGEMENTS

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REFERENCES