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Dynamic behaviour of $\beta$-Ti-15333 in ultrasonically assisted turning: Experimental and numerical analysis

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KEYWORDS
Ti-alloys;
SHPB;
Turning;
Machining;
Finite-element.

Abstract. The enhanced strength, fatigue life, and corrosion resistance properties of Ti-alloys have attracted many industries for their utilization in various components exposed to extreme operating conditions. The machining of these alloys using conventional machining techniques is one of the main challenges in its wide application in many components, and there is an obvious demand to analyse the materials’ response to these alloys in machining processes by developing simulation-based models. The materials’ behaviour used in simulation of machining processes is usually determined by means of Split-Hopkinson-Pressure-Bar (SHPB) setup. A 3D thermo-mechanically coupled Finite-Element (FE) model of SHPB is developed in the current work to analyse materials response of $\beta$-Ti-15333 at the selected temperature, strain rate, and strain. The obtained materials’ response to the tested alloys is used in 3D thermo-mechanically coupled FE model of ultrasonically assisted turning and conventional turning at various tested cutting conditions. The developed FE model is used for parametric analysis of $\beta$-Ti-15333 machining, and the obtained FE results are in good agreement with experimental results.

1. Introduction

The machinability of $\beta$-Ti-alloys is characterised by high level of cutting forces and extreme temperature at the process zone in machining processes due to its low thermal-conductivity and high-strength [1-4]. The produced plastic deformation in $\beta$-Ti-alloys in Ultrasonically Assisted Turning (UAT) and Conventional Turning (CT) results in the high level of temperature, strain rate, and strain in the process zone. The level of strain rate in moderate speed machining of hard-to-cut alloys usually reaches $10^2$ s\textsuperscript{-1} to achieve material separation. The accurate incorporation of these high level strain rate and temperature-dependent behaviours of material used in Finite-Element (FE) simulation is the vital and critical step in numerical analysis of machining processes [5,6]. Among many, Split-Hopkinson-Pressure-Bar (SHPB) setup is one of the commonly used experimental techniques to determine materials’ response at elevated strain and strain-rate levels. The method is useful for the prediction of materials’ response at the strain rate levels, ranging from $10^1$ to $10^4$ s\textsuperscript{-1}. However, the strain rate level in machining process at the primary and secondary deformation zones surpasses the achieved levels in SHPB tests and, therefore, cannot be used in the FE simulation of machining processes.

The data obtained from SHPB tests are based on some basic approximations, containing the practice of uniformity of strain and stress used in 1D-theory
of elastic wave spread, evenness of strain, and stress
distribution in the direction of the axis of the wave
propagation and the ignoring of the frictional effect.
The details of the studied effects of these parameters
on the obtained results of SHPB tests are available
elsewhere [7]. These assumptions are critically assessed
by various researchers worldwide, both numerically and
experimentally, and the advantages and disadvantages
of SHPB tests are highlighted [8-11].

In the past, researchers used Johnson-Cook
(JC) [12] model, which is a curve fitting technique to
predict materials response at higher strain rate, strain
and temperature used in FE simulation of machining
processes [10,13-17]. The model has the capability to
represent materials’ response accurately in machining
operations and produce precise results in FE simulation
with the achieved experimentations. However, there
are other materials’ models also available in the lit-
erature that need to be tested in the FE simulation
of machining processes. In the current study, a
piecewise linear material model is used to incorporate
the materials response at these higher strain rates,
temperatures, and strains. The main limitation of the
piecewise linear material model is that it needs tested
material response at $10^2$ s$^{-1}$ for machining simulations,
which is not the case in the current study. Therefore,
there is a need to use advanced FE tools to predict
materials’ response at those high strain rate levels, and
then used it in FE simulations of machining processes.

Hence, the data obtained from experimentations
of the SPHB tests were verified with a developed
3D FE model of SPHB setup at the studied lev-
els of strain, temperature, and strain rates. The developed model was also used to investigate the
deforation mechanism of $\beta$-Ti-15333 alloy at the
tested loads of various combinations of temperatures
and strain rates. Later on, the model was used to
extrapolate the achieved materials’ response from
SHPB tests to the required level of strain rate
reached in machining processes to accurately repres-
ent materials’ response in FE simulation of $\beta$-Ti-
15333.

Moreover, a coupled 3D thermo-mechanically FE
model of UAT and CT was established to carry out
parametric study of $\beta$-Ti-15333 at various cutting
conditions. The developed model was examined for
the level of cutting forces, stresses, and temperature
induced in the process zone at various tested condi-
tions.

2. SPHB tests

The SPHB setup used in the current work consists of
two managing steel rods: transmitted bar and incident
bar, each with diameter lengths of 1200 mm and
21.77 mm, as shown in Figure 1. A striker rod having
the same diameter as that of incident rod and length of
200 mm is used as a source to apply load to the incident
bar from the pressurized cylinder. $\beta$-Ti-15333 sample
used in the SPHB tests with a diameter of 8 mm and
6 mm length is mounted between the incident and
transmitted rods. The resistance strain gauges are
fixed on the incident and transmitted rods to measure
the response of $\beta$-Ti-15333 due to the applied load.
The load is applied to the incident rods with a striker
rod at the certain level of strain rate and is spread
throughout the specimen (see Figure 1). The propagated
pulse from the incident rod is divided into two streams,
then reaches the mounted sample. A part of pulse
travels through the sample and reaches the transmitted
rod because of plastic deformation, and the resistance
strain gauges attached to it record the levels of those
stresses. Similarly, an elastic pulse reflected back to the
incident rod from $\beta$-Ti-15333 specimen is noted by the
mounted strain gauge on it. A 1D-wave propagation
theory is applied to define the level of stress, strain rate,
and strain in $\beta$-Ti-15333 specimen from the achieved
experimental data. The details are given below [18]:

$$\varepsilon(T) = -\frac{2B}{l_s} \int_0^T \varepsilon_R(T) \, dt,$$

$$\dot{\varepsilon}(T) = -\frac{2B}{l_s} \varepsilon_n(T),$$

$$\sigma(T) = \frac{a_b E_b}{a_s} \varepsilon_T(T),$$

Figure 1. Block diagram of SPHB experimental setup used in the study.
where $B$ is the velocity of elastic wave, $l_s$ is the specimen initial length, $\varepsilon_T$ and $\varepsilon_R$ are the strain pulse levels of transmitted and reflected waves, respectively; $a_s$ and $a_b$ are $\beta$-Ti-15333 specimen and rods cross-sectional areas, respectively. $E_b$ is the elastic-modulus of the rod materials, $\varepsilon(T)$ represent the strain rate, $\varepsilon(T)$ is the level of strain, and $\sigma(T)$ represents the level of the resulted stresses.

$\beta$-Ti-15333 specimen was prepared using a wire cut machine to achieve length-to-diameter ratio within the range of 0.5 to 1. The length-to-diameter ratio of $\beta$-Ti-15333 specimen used in the tests was 0.75. The tests were conducted at 0.1, 1, 600, 1300, and 3300 s$^{-1}$ strain rate levels as shown in Figure 2. Similarly, tests at various temperature levels of 20°C, 600°C, 800°C, and 950°C were also carried out to achieve $\beta$-Ti-15333 response (see Figure 3) [19]. A decline in the strength of the studied materials was observed at elevated temperature, as expected.

3. Machining tests

The conventional lathe machine (Harrison-300) modified to mount the piezo-ceramic transducer on the tool post was used in the current study. A custom-built fixture was fabricated to fix the designed transducer on the lathe machine and cutting inserts were fixed on the free end of the transducer. The developed ultrasonic system at Loughborough University, UK, is an open loop system optimized for vibrational parameters of 8 µm amplitude and 20 kHz frequency. The system is also designed in such a way as to carry out both CT and UAT by simply switching on the ultrasonic vibration on the cutting tool. A dynamometer of Kistler type offers the measured level of cutting forces in real time at the studied cutting parameters. The data obtained from the dynamometer were passed through a data acquisition system, and response of the cutting forces was recorded. For thermal analysis of the process zone, a FLIR Thermacam™ SC-3000 system was used to calculate the process-zone temperature in UAT and CT. The thermal camera was calibrated in the lab before conducting the tests on the studied alloys. The data obtained in experimentation were further analysed using the Thermacam® QuickView™ software. Figure 4 shows the experimental setup used for CT and UAT of $\beta$-Ti-15333.

3.1. Cutting insert and workpiece materials in turning tests

A 500 mm length and 60 mm diameter ingot of $\beta$-Ti-15333 was used in UAT and CT tests. $\beta$-Ti-15333 rod was attached to the chuck of the lathe-machine and eccentricity of the work piece was adjusted using a mechanical dial gauge. All tests were conducted in dry-cutting conditions. The cutting inserts used in the experimentation were DNMG150008 manufactured by SECO. The tested cutting conditions in turning experiments are shown in Table 1 and is recommended for $\beta$-Ti-15333 alloy by the funding agency for the current work. Additional details about $\beta$-Ti-15333 alloy can be found elsewhere [20].

4. FE models

4.1. SHPB model

A 3D FE model for SHPB was developed in MSC MARC-MENTAT as shown in Figure 5 to predict the materials’ behaviour at strain rate levels observed in machining processes. The achieved experimental data from the SHPB tests represent $\beta$-Ti-15333 response up

<table>
<thead>
<tr>
<th>Cutting parameters</th>
<th>Magnitude</th>
</tr>
</thead>
<tbody>
<tr>
<td>Depth of cuts</td>
<td>100-500 µm</td>
</tr>
<tr>
<td>Feed rate</td>
<td>100 µm/rev</td>
</tr>
<tr>
<td>Cutting speed</td>
<td>10-70 m/min</td>
</tr>
<tr>
<td>Lubricant</td>
<td>Dry cutting</td>
</tr>
</tbody>
</table>
to a maximum of 3300 s⁻¹ due to the limitation of the setup used. The specimen used in SHPB tests, incident, striker and transmitted rods was modelled using 8-node hexahedral and isoparametric elements available as element type 7 in the MSC MARC library as per the dimension presented in Table 2. The striker and transmitted rods were allowed to move in the direction of the shaft axis, and reflected rod was constrained in this direction to replicate the effect of stopper on it. The materials’ properties, available in Table 2, were assigned to SHPB setup bars and the achieved data from SHPB tests used in the model for β-Ti-15333 specimen using a piecewise linear materials model (Eq. (4)) with slight modification to eliminate the convergence problems faced in FE simulations, as shown in Figure 6.

$$\sigma = \sigma (\varepsilon, \dot{\varepsilon}, T)$$,

where \(\sigma\) is the yield stress, \(\varepsilon\), \(\dot{\varepsilon}\), and \(T\) are the strain, strain rate, and temperature, respectively.

**Figure 5.** The developed FE model of SHPB [23].

**Figure 6.** Modification in SHPB data to eliminate variation and convergence problems in FE simulations.

### 4.2. FE modelling of UAT and CT

A 3D FE model of UAT and CT was developed in MSC MARC-MENTAT, as shown in Figure 7. A deformable β-Ti-15333 workpiece having a width of 1.3 mm, length of 5 mm, and 0.5 mm + \(a_p\) height was modelled using 8-node hexahedral elements. The initially used 8-node elements were changed to 5-node tetrahedron elements using global remeshing technique to elude excessive deformation in the workpiece and chip separation. The cutting insert having 800 \(\mu\)m nose radius, 14.5° rake angle, 25 \(\mu\)m cutting edge radius, and 0° end relief angle was developed in Pro-Engineer and exported.

### Table 2. Mechanical properties and dimensions of rods/specimen used in the SHPB system.

<table>
<thead>
<tr>
<th>Material</th>
<th>Length, (l) (mm)</th>
<th>Diameter, (d) (mm)</th>
<th>Modulus of Elasticity (GPa)</th>
<th>Poisson’s ratio</th>
<th>Density (kg/m³)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Striker rod</td>
<td>200</td>
<td>21.77</td>
<td>198</td>
<td>0.329</td>
<td>8470</td>
</tr>
<tr>
<td>Bars</td>
<td>1200</td>
<td>21.77</td>
<td>198</td>
<td>0.329</td>
<td>8470</td>
</tr>
<tr>
<td>Specimen</td>
<td>6</td>
<td>8</td>
<td>87</td>
<td>0.3</td>
<td>4900</td>
</tr>
</tbody>
</table>
frictional-stress, $\sigma$ is the level of equivalent stress, $V_r$ is a sliding critical-velocity for sticking activation, $m_{fr}$ represents the coefficient of friction, and $\text{sgn}(x)$ is the signum function.

The chip separation from the workpiece in the FE simulation of UAT and CT was achieved through global remeshing technique, built into the feature of MSC MARC Mentat.

5. Discussions on results

5.1. FE results of SHPB

The developed FE model of SHPB was used to calculate the axial-strain level at the desired point on the bar where the resistance strain gauge was mounted, as shown in Figure 9. A propagation of compressive strain in the incident rod was observed when the striker rod smashed it. A rapid increase of 0.04 in the incident rod at strain level was observed when the striker fully hit it. The level of strain started to decay and reached the lower level of strain at 0.14 s before the plastic deformation of the specimen was placed between the incident and transmitted rods. The specimen's plastic deformation response in the reflected and transmitted pulses was achieved in incident and transmitted rods, respectively. The model was used for various strain rate levels of deformation of the tested specimen, and reasonably good agreement between the experimental and FE results was accomplished. Figure 10 shows the response of $\beta$-Ti-1533 both experimentally and numerically at the strain rate level of 3300 s$^{-1}$.

At the start of the compression of the specimen, inconsistent plastic deformation was observed in the studied $\beta$-Ti-1533. The homogenous state of the stress was achieved at 3% of strain in the FE results. A total variation of approximately 138 MPa in the axial stress was observed at the initial contact between the incident bar and sample, as shown in Figure 11. Similarly,
the variations in equivalent stresses are in the range of approximately 400 MPa and reached homogenous state at 30 μs, as shown in Figure 12. These results violate the approximation taken in the SHPB tests, stating that the levels of stresses in the axial direction are homogeneous.

Similarly, a non-uniform distribution of temperature was observed at the initial interaction of the incident bar and specimen (see Figure 13). A growth of 117°C was observed in the sample due to low thermal conductivity of the tested samples, severe plastic deformation, and adiabatic heating conditions.

The developed FE model of SHPB was mainly used to predict the materials’ response at high strain-rate levels in the current study. The model was simulated to interpolate the materials’ response for the known experimentally obtained strain rate levels based on the extrapolated assumed materials’ response at higher strain rate. An engineering assumption was used to extrapolate the materials’ response at 10¹⁰ s⁻¹, which is 20% higher than the measured level of stress-strain response at 3300 s⁻¹. The interpolated material response of the studied material at 3300 s⁻¹ is presented in Figure 14 [6,21,22]. The level of stresses obtained from the FE model was lower than the actual materials’ response obtained from SHPB test. The same assumption was also made for the strain rate level of 10⁸ s⁻¹ and reasonably good agreement between the experimental and interpolated FE results was obtained at 1300 s⁻¹ strain rate. The only problem with the achieved FE results was the lower strain level compared to the experimental results, however, to avoid convergence issues caused by the negative slope of materials’ response in the FE modelling of UAT and CT, the same level of stress was assumed as a strain
level of 0.4. The same approximation was tested at various temperature levels, and the achieved results were in reasonably good agreement with the validated experimental results.

The obtained results of FE model of SHPB setup were used in the FE model of UAT and CT to incorporate materials’ response at the strain-rate level of $10^2$ s$^{-1}$. Although the additional outcomes of inhomogeneity in the stress, strain, and growth in temperature were not incorporated into the current study, a detailed analysis of actual response of materials in SHPB tests was obtained.

5.2. Analyses of UAT and CT results
The FE simulations of UAT and CT at various cutting conditions were conducted with the developed FE model and all three-component forces were obtained. In CT of β-Ti-15333, a magnitude of 110 N was observed for tangential force components ($F_\tau$) at 10 m/min speed and 300 µm depth of cut. Similarly, the magnitudes of radial force component ($F_r$) and axial force components ($F_z$) of 48 N and 20 N, respectively, were observed (see Figure 15).

The cutting edge was in continuous connection with the workpiece materials after the initial engagement in CT and a uniform level of cutting forces was detected. The small fluctuation in the observed forces is ascribed to the remeshing technique used for chip separation. On the other hand, in UAT, the alternating contact between the cutting insert and the workpiece oscillated the cutting forces between the maximum and minimum levels as presented in Figure 16. The level of cutting forces is almost zero at the approach stage and retraction stage of the cutting insert movement in one complete cycle. The level of cutting forces started to increase at the initial connection between the cutting insert and workpiece during the penetration stage. The level of forces approximately reached the peak force level observed in CT, and then started to decline and reach zero level when the tool was separated from the chip. Hence, a noteworthy decline in the average level in cutting forces was achieved in UAT compared to CT in the same cutting conditions.

As a result, the average level of $F_z$ dropped from 110 N to 35 N in UAT. In addition, a considerable decline of 68% and 55% in the levels of $F_y$ and $F_z$ was achieved.

The FE model was used to carry out simulations at the tested depths of cut and a gradual growth in the levels of $F_x$, $F_y$, and $F_z$ was observed with a growth in the depth of cut in both UAT and CT, as expected. The variation of cutting forces in CT with the depth of cut is presented in Figure 17. The obtained results from the FE model validated the experimental results.

Similarly, the results shown in Figure 18 present the changes in the cutting forces for various depths of cuts in UAT. The depths of cuts varied from 100 µm to 500 µm and an approximately linear growth in $F_x$, $F_y$, and $F_z$ was noted with it in UAT. The attained simulation results showed excellent agreement with those of the calculated experimental data in UAT. The obtained simulation results in UAT showed an approxi-

![Figure 15](image_url). Level of cutting forces calculated in FE simulation of CT at 10 m/min, 300 µm depth of cut and 100 µm/rev feed rate.

![Figure 16](image_url). The history of cutting forces in one complete cycle of UAT.

![Figure 17](image_url). The Level of cutting forces in CT at various depths of cut.
approximately 65-72% reduction in $F_x$. Similarly, a significant reduction of approximately 70% and 50% decline in $F_y$ and $F_z$ was achieved, respectively. The decrease in $F_x$, $F_y$, and $F_z$ can be ascribed to the separations of insert from the workpiece during retraction stage of tool movement in one complete vibrational cycle as reported. Further analyses showed that the average level of $F_x$ in UAT at 500 μm is approximately equal to the force levels observed in CT at 100 μm. Hence, for the equal magnitude of cutting forces, UAT increased the machinability of the studied alloy approximately 5 times when compared to CT.

Furthermore, the effect of cutting speeds going from 10 m/min to 70 m/min on cutting forces was also analyzed through the developed FE model. Figure 19 presents the cutting forces obtained at the tested speeds in CT. The levels of $F_x$, $F_y$, and $F_z$ were approximately the same for various cutting speeds. On the other hand, a growth in $F_x$, $F_y$, and $F_z$ with cutting speeds was observed in UAT and lasted up to 70 m/min. This growth disappeared beyond 70 m/min, as the work piece’s velocity was high enough to exclude separation between the workpiece and tool in one cycle of ultrasonic vibration (see Figure 20). In UAT, at 60 m/min which is the critical velocity of vibrating tool, a drop of approximately 10% is noted in the level of $F_x$ as compared to CT and was ascribed to the thermal softening produced in the process zone in UAT due to the process zone temperature. The obtained FE results validated the experimental data presented by Maurotto et al. [20].

The assessment results of the obtained $F_x$, $F_y$, and $F_z$ at various feed rates in UAT and CT are displayed in Figure 21. A growth in $F_x$, $F_y$, and $F_z$ was noticed with intensification in feed rate of both turning processes. The quantity of the removed material by the insert at higher feed-rate increases, resulting in higher levels of $F_x$, $F_y$, and $F_z$ on the insert.

At feed rates of 0.2 and 0.3 mm/rev, a reduction of approximately 60% was observed in $F_x$ and $F_y$ in UAT. However, with an increase in feed rates, the reduction in $F_z$ diminished, and 24% reduction was observed at
0.3 mm/rev. The decline in the drop of \( F_z \) in UAT is due to a tinier separation of insert at the retraction stage, resulting in a higher average force on the insert. However, the reduction in the levels of \( F_x \) and \( F_y \) was noticeable, and hence UAT was also effective at higher levels of feed rate.

The process zone temperature was studied both experimentally and numerically in both UAT and CT, as shown in Figure 22. The observed temperature at the process zone from FE model was slightly higher compared to the level of temperatures observed in experimentations [24,25]. The process zone was obstructed by the chip formed in both UAT and CT, and hence resulted in a lesser assessment of the temperature of the process zone. Still, the temperature level of process zone visible to the line of sight of the infrared camera shows excellent agreement with the acquired FE outcomes. The developed FE model predicts the temperature of those regions, which cannot be examined with experimentations.

Relatively higher temperature at the process zone of approximately 100°C was achieved in UAT both numerically and experimentally. The forced vibration on the insert resulted in a comparatively higher velocity (60 m/min) of the cutting edge in the penetration stage; hence, that is responsible for this growth in temperature [1,3,11,13,15].

Similarly, the developed FE model was used for the spreading of von-Mises stress in the studied zone of UAT and CT, as shown in Figure 23. The distribution of stresses was uniform in CT due to the continuous contact of the cutting tool with the workpiece materials. The maximum level of stress observed in the process zone was approximately 1055 MPa in CT. On the other hand, a transient distribution of stresses in the process zone was calculated in UAT due to the intermittent contact of the cutting edge and workpiece material. The level of stresses reached approximately 1050 MPa at the penetration stage and started to decline to the minimum level at the retraction stage when the cutting edge was completely detached from the workpiece and chip. The level of average stresses observed in one complete cycle of UAT is significantly lower compared to the level of stresses observed in CT. However, the level of stress reached the level observed in CT for a fraction of time during the penetration stage.

Furthermore, the FE model was also used to predict the level of strain rate induced in UAT and CT of Ti-15333, as displayed in Figure 24. The level of strain rate calculated at the penetration stage in UAT was considerably higher than that observed in CT. The vibration supplied to the cutting tool resulted in transient contact with the workpiece material, and hence resulted in a four-time increase in the level of strain rate in UAT.

6. Conclusion

The FE model was developed for SHPB setup to investigate the behaviour of Ti-15333 at various strain-rate.
strain, and temperature. The developed model was validated by the available experimental data. The model was used to predict Ti-15333 behaviour at the elevated strain rate of $10^6 \text{ s}^{-1}$. The deformation behaviour was inhomogeneous for Ti-15333 at the initial stages of compression in SHPB simulations, contradicting the main assumption made for stress-strain response calculation of the SHPB tests. Similarly, a growth in temperature of the specimen due to adiabatic heating condition was also observed. These observations should be taken into consideration for future calculation of Ti-15333 materials model's parameters.

The obtained materials' response of Ti-15333 at higher strain from the SHPB simulation was used in the thermos-mechanically coupled FE model of UAT and CT. The developed model has an added advantage of predicting $F_x$, $F_y$, and $F_z$ in both UAT and CT. A significant drop of approximately 70% in the level of $F_x$ was observed. The model is also capable of explaining the reduction in the level of $F_y$ and $F_z$ in UAT. The FE results show that UAT is effective in both higher feed rates and depth of cuts, resulting in a significant drop in all the three components of forces. The observed temperature at the process zone is relatively high in UAT. The predicted FE results are in good agreement with the validated experimental results.

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